



# TESTING & STANDARDIZATION PANEL SESSION: SPEC PROPOSAL FOR NANOCRYSTALLINE CMC

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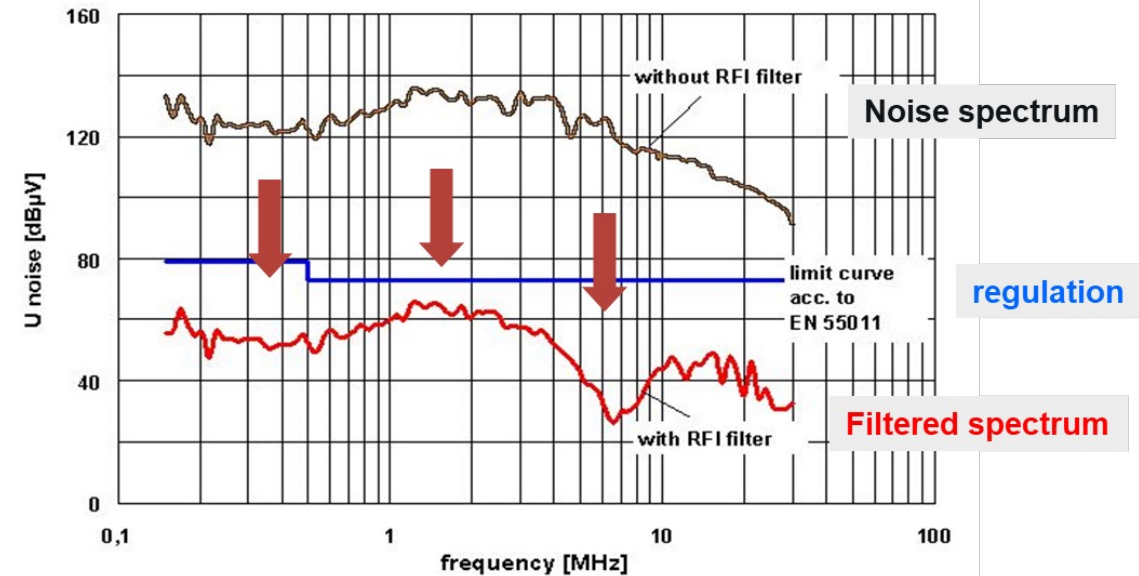
## Nanocrystalline material vs Ferrite

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Material	Nanocrystalline (VITROPERM®)	Ferrite
Material base	~ 70% Fe	MnZn (NiZn)
Coercivity $H_c$ [A/m]	<3	5...60 (...2000)
Losses $P_{Fe,ty p.}$ [W/kg] 100 kHz, 300mT, 100°C	60...90 (VP500) 40...50 (VP550HF)	140
Saturation flux density $B_s$ [T]	> 1.2 (room temp.) ca. 1.1 (120°C)	< 0.48 (room temp.) ca. 0.3 (120°C)
Initial permeability $\mu_i$	2000...200 000	10...10 000 (20000)
Saturation magnetostriction $\lambda_s$	$10^{-7} \dots 10^{-8}$	$10^{-6} \dots 2 \times 10^{-5}$
Max. operating temp. $T_{op}$	plastic case 130°C* core 155°C, 180°C (short time)	< 100°C (120°C)
Curie temperature [°C]	> 600	150...200

- How much attenuation of noise is needed?  
**Required impedance**
- Over what frequency bandwidth is the noise?  
**Required frequency range**
- How much current must it handle?  
**Required current handling**

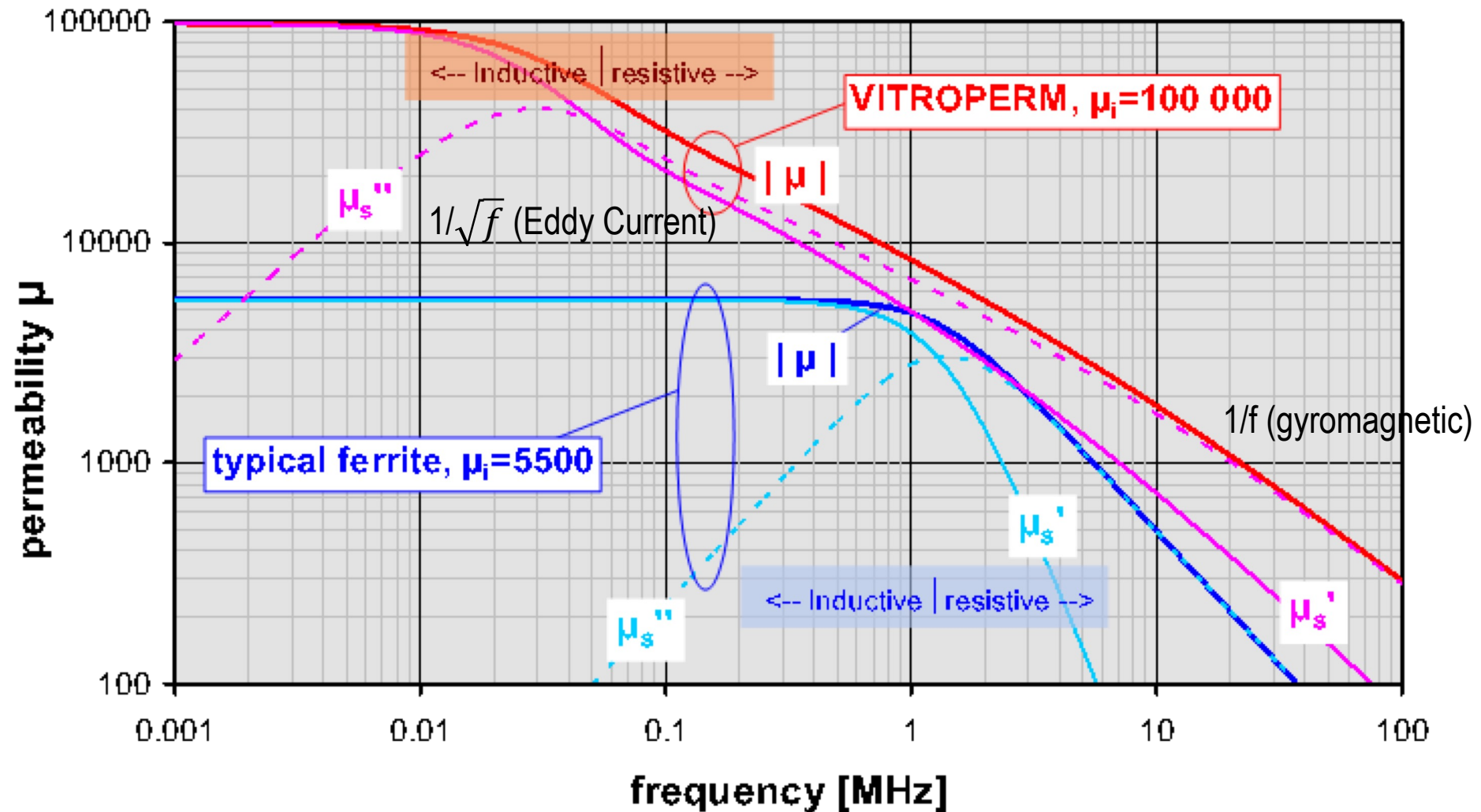
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- ❖ |Z| and L measurement in a normal Impedance Analyzer provides the basic information to calculate permeability, power losses, etc.
- ❖ Proposed range to measure is 100Hz thru 100MHz (ferrites can't effectively function as CMC above 2MHz without significant limitations in size, DC tolerance, temperature dependence, etc.).

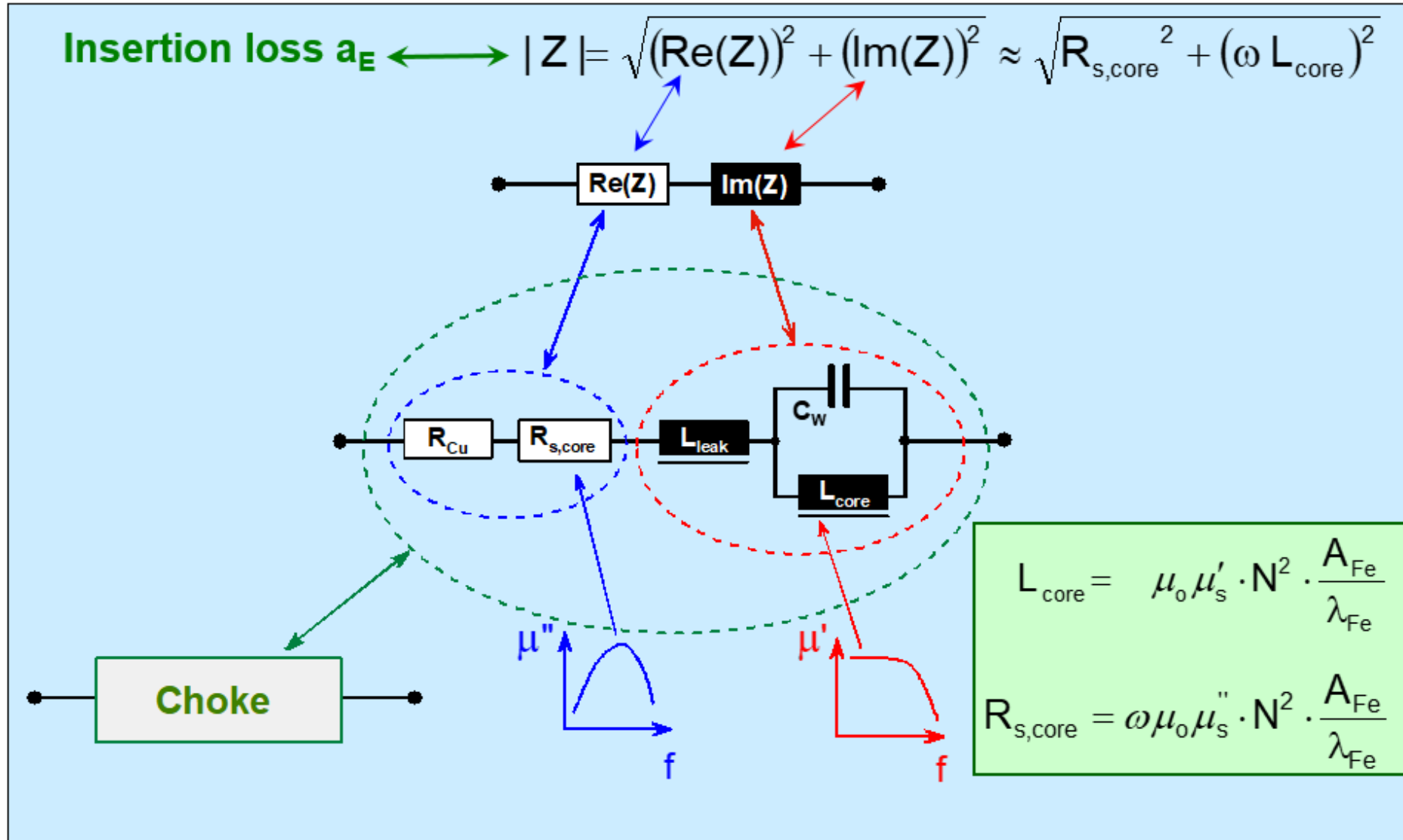
# FREQUENCY DEPENDENCY OF PERMEABILITY

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## Choke: $|Z|$ - equivalent circuit - $\mu'$ , $\mu''$

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VAC recommendation is to measure  $|Z|$  (complex impedance) and  $L$  (inductance) between 100Hz and 100 MHz

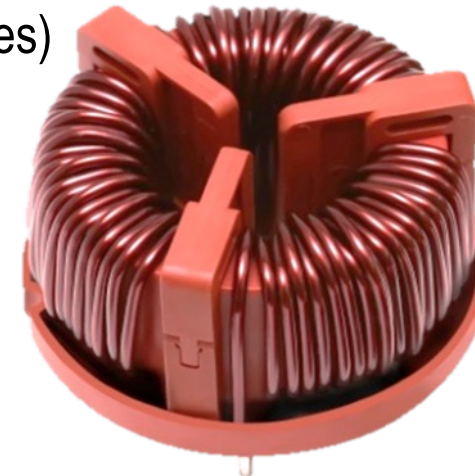
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1.  $L$  (10 kHz)  $\rightarrow$  comparison with ferrite
2.  $L$  (100 kHz)  $\rightarrow$  real focus for the application
3.  $|Z|$  (f)  $\rightarrow$  insertion loss can be calculated
4.  $L_s$  (Leakage inductance)  $\rightarrow$  interesting to understand the DM attenuation (usually better in ferrites)
5.  $I_{unbal}$  (DC, 10kHz, 100kHz)

Betriebsdaten/Charakteristische Daten (Typische Werte):  
Operational data/characteristic data (typical values):

	f=10kHz	f=100kHz	DC
$L$ [mH]	16,9	3,6	
$ Z $ [ $\Omega$ ]	1300	4000	
$I_{unbal.}$ [mA]	22	45	19

$L_s / L_{leak} = 16 \mu\text{H}$  and  $f = 100 \text{ kHz}$  (Eine Wicklung kurzgeschlossen / one winding shorted)  
Bemessungsisolationsspannung / rated insulation voltage:  
 $U_{is} = 600 \text{ V}_{RMS}$  (848  $V_{peak}$ ) (Netzstromkreis / connected to the mains)  
 $1000 \text{ V}_{RMS}$  (1414  $V_{peak}$ ) (Nicht-Netzstromkreis / not connected to the mains)  
 $I_N = 2 \times 13.5 \text{ A}$   $m = 54 \text{ g}$   
Umgebungstemperatur / ambient temperature:  $T_a = -40^\circ\text{C} \dots +70^\circ\text{C}$   
Lagertemperatur / storage temperature:  $T_{st} = -40^\circ\text{C} \dots +85^\circ\text{C}$



Extracted from an existing VAC datasheet



# SPEC RECOMMENDATION (PART 2)

- The graph L vs DC current bias must be as rectangular as possible (optimized performance). This graph helps calculate permeability:

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With

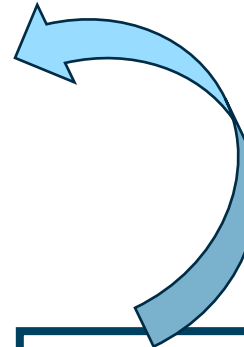
L=Inductance

N=Number of turns

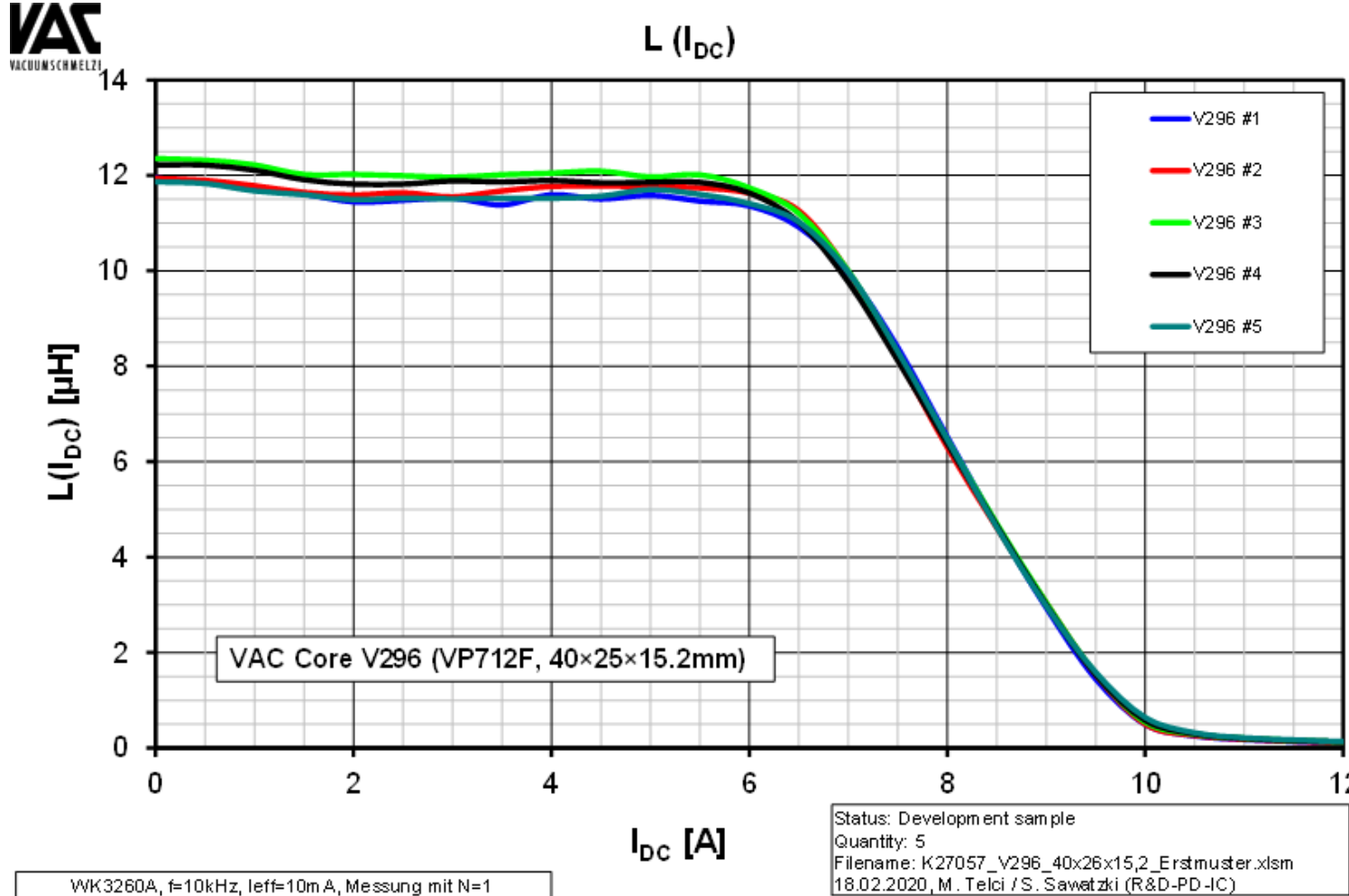
$l_{Fe}$ =Iron path length

$A_{Fe}$ =Iron cross section

you get: 
$$\mu' = \frac{l_{Fe}}{\mu_0 \cdot A_{Fe}} \cdot \frac{L}{N^2}$$



Maximum common mode current can be calculated from 70% of value at ( $I_{dc} = 0$ )



# SPEC RECOMMENDATION (PART 3)

Further recommendations to specify a superior solution...

- Include a tighter tolerance +/- 6%:
    - ❖ For core weight
    - ❖ For  $A_{fe}$
  - The purpose is to reduce the scattering of the filling factor and tight the inductance range.
  - An excellent CMC should be able to reach higher DC tolerances for the same amount of material.
- The narrower the temperature dependency of the magnetic characteristics, the better performance the CMC will show across the temperature range. Interesting hint for the designer to make a good selection.



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